ประสิทธิภาพการดูดซับด้วยถ่านชีวภาพยูคาลิปตัสแบบยึดติดคอลัมน์เพื่อกำ จัดแมงกานีส ในน้ำ บาดาล

Adsorption performance of eucalyptus biochar fixed-bed column for manganese removal from groundwater

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บทคัดย่อ

การกำ จัดแมงกานีสในน้ำ ใต้ดินปนเปื้อนด้วยระบบการกรองเป็นระบบที่นิยมใช้มากที่สุด งานวิจัยนี้มีวัตถุประสงค์เพื่อศึกษา ประสิทธิภาพของคอลัมน์แบบยึดติดกับที่ ที่ใช้ถ่านชีวภาพยูคาลิปตัสและถ่านชีวภาพยูคาลิปตัสที่ปรับปรุงพื้นผิวด้วยด่างทับทิม เป็นสารกรองในการกำ จัดแมงกานีสจากน้ำ ใต้ดินที่ความเข้มข้น 0.723 + 0.002 มก./ลิตร โดยป้อนน้ำ เข้าสู่ด้านบนของคอลัมน์ กรองระดับห้องปฏิบัติการอย่างต่อเนื่องอัตราการไหล 5 ลิตร/วัน เก็บตัวอย่างน้ำ ที่เวลาต่างๆ จนครบ 24 ชั่วโมง ใช้แบบจำ ลอง โธมัสและยุน-เนลสัน เพื่ออธิบายความสามารถในการดูดซับแมงกานีส ผลการศึกษาพบว่าถ่านชีวภาพยูคาลิปตัสมีความสามารถ ในการดูดซับเท่ากับ 1.812 มก./กรัม สูงกว่าถ่านชีวภาพยูคาลิปตัสที่ปรับปรุงพื้นผิวเนื่องจากมีค่าไอโอดีนนัมเบอร์สูงกว่า โดยความสามารถในการดูดซับเท่ากับ 0.769 มก./กรัม และเวลาดูดซับที่ร้อยละ 50 ของเบรคทรูของถ่านชีวภาพยูคาลิปตัส และถ่านชีวภาพ ยูคาลิปตัสที่ปรับปรุงพื้นผิวมีค่าเท่ากับ 1,020 และ 240 นาที ตามลำดับ มีความสอดคล้องกับแบบจำลองของ ยุน - เนลสัน การใช้ EB และ MEB เป็นวัสดุกรองจากท้องถิ่นสามารถลดต้นทุนการปรับปรุงคุณภาพน้ำให้กับชุมชนได้

คำ สำ คัญ: ตัวกรองถ่านชีวภาพ แมงกานีส คอลัมน์แบบยึดติดกับที่ น้ำ บาดาล ยูคาลิปตัส

Abstract

Removal of manganese in contaminated groundwater using filtration is one of the most treatment systems. The objective of this research was to study the efficiency of fixed-bed adsorption column using eucalyptus biochar and potassium permanganate-modified eucalyptus biochar as filter media to remove manganese from groundwater. The initial manganese concentration of 0.723 ± 0.002 mg/L was continuously fed to the top of column at a flow rate of 5 L/d. Water samples were collected periodically within 24 hours. Thomas and Yoon-Nelson models were used to describe the adsorption performance. Results showed that adsorption capacity of eucalyptus biochar was 1.812 mg/g higher than that of modified eucalyptus biochar (0.769 mg/g) as it has higher iodine number. The adsorption times at 50% breakthrough of eucalyptus biochar and modified eucalyptus biochar were 1,020 minutes and 240 minutes, respectively, which were consistent with the Yoon-Nelson model. Use of EB and MEB as local filter media can reduce the cost of improving community water quality.

Keywords: Biochar filter, manganese, fixed-bed column, groundwater, eucalyptus

หลักสูตรเทคโนโลยีสิ่งแวดล้อม คณะพลังงานสิ่งแวดล้อมและวัสดุ มหาวิทยาลัยเทคโนโลยีพระจอมเกล้าธนบุรี กรุงเทพฯ 10140
กลุ่มวิจัยการจัดการสิ่งแวดล้อมและพลังงานเพื่อชุมชนและเศรษฐกิจหมนุเวียน มหาวิทยาลัยเทคโนโลยีพระจอมเกล้าธนบุรี

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Introduction

Groundwater represents 97% of the world's available freshwater resources (Guppy *et al*., 2018). It is used widely, especially in developing countries in Asia such as Thailand. People in the northeastern region use groundwater because most areas are not in the service area of the Provincial Waterworks Authority. Groundwater quality is dependent on geologic conditions and human activities. Groundwater resources can be contaminated naturally by salt intrusion, and human activities *via* agriculture practices, and heavy metal contamination from industries (Vesselinov *et al*., 2018). In the Chi and Mun river basins, groundwater has iron, manganese, sulfate and fluoride concentrations exceeding the maximum allowable limits of groundwater standards for drinking water. In some areas of Ubon Ratchathani Province, there are high iron and manganese concentrations in groundwater more than 1 mg/L (Department of Groundwater Resources, 2022). Manganese in groundwater is found as the dissolved form of manganese bicarbonate $(Mn(HCO₃)₂)$. As groundwater is exposed to air, the dissolved form is oxidized to dark brown insoluble manganese (Mn(IV)) (Henry & Heinke, 1989). This causes the appearance in stored water of a black sediment from manganese, causing stains to sanitary equipment and which may also affect health due to it being a chronic toxin (Rahman *et al*., 2021 ; Schullehner *et al*., 2020 ; Tay *et al*., 2018).

Manganese could be removed by physical, chemical, biological and physicochemical processes (Patil *et al*., 2016). The common and popular methods are the physical processes of adsorption and filtration. Activated carbon is most frequently used as solid adsorbent because it is a very effective adsorbent in various applications (Yin *et al*., 2007). The high surface areas and functional groups of activated carbon could remove Mn(II) from water (Chen *et al*., 1996). Previous research has used a variety of adsorbents such as activated carbon derived from Ziziphus spina-christi seeds (Omri & Benzina, 2012), kaolin (Yavuz *et al*., 2003), manganese oxide-coated zeolite (Alvarez-Bastida *et al*., 2018) and greensand or manganese oxide-coated sand (Benis *et al*., 2020). Potassium permanganate (KMnO_4) is an oxidizing agent. It has been reported to be an efficient oxidant to achieve

manganese removal of 96% from groundwater (Menard & Demopoulos, 2007). Thus, KMnO₄ is widely used as a material coating on adsorbents. Most conventional wastewater treatment plants use manganese oxide-coated media to remove soluble manganese and then subsequent oxidation by free chlorine to $\mathsf{MnO}_x(\mathsf{s})$ (Hargette & Knocke, 2001). The filtration method is suitable for rural areas to remove heavy metals and odorous compounds before the distribution system. The filtration process in the community normally uses a combination of sand, anthracite or activated carbon as filter media. The problem encountered with rural filtration systems is the excessive cost of filter media. Thus, biochar can be an alternative low-cost filter media for heavy metal removal. Previous studies have reported the use of biochars for manganese removal in batch experiments with, for example, poultry manure and farmyard manure-derived biochar (Idrees *et al*., 2018), palm waste-derived biochar (Fseha & Yildiz, 2022), and biochar made banana peel and acid-modified banana peel (Kim *et al*., 2020). However, limited documentation is available for heavy metal removal using real groundwater in column studies.

Eucalyptus is an economic crop in Thailand because it is a fast-growing plant, widely cultivated for a variety of uses. Eucalyptus branches are highly productive as charcoal and have low cost. In addition, eucalyptus biochar (EB) has been used as an adsorbent for lead removal in aqueous solution (Singh & Arora, 2018) and manganese in groundwater (Wilamas *et al*., 2022). Activated carbon derived from eucalyptus was reported as effective for removal of cadmium (Venkatesan & Rajam, 2014). However, the removal of manganese in groundwater by eucalyptus biochar filter including modified surface-biochar by KMnO_4 . has not been reported in any specific studies. Thus, this research used eucalyptus to produce biochar and its surface modification for manganese removal from groundwater. The objectives were to determine the efficiency of fixed-bed adsorption columns filled with eucalyptus biochar and modified eucalyptus biochar (MEB) for manganese removal from groundwater and use of the Thomas and Yoon-Nelson models for prediction of the adsorption performance.

Materials and methods

1. Preparations of filter media

Eucalyptus biochar was produced using ground pits. The eucalyptus branches were cut to a length of 50 cm and put in a hole dug in the ground $(60 \times 90 \text{ cm})$. Then, it was covered and burnt slowly with limited of oxygen on the top using auxiliary fuel (wood chips) for 6 hours. The temperature was between 400 - 500 °C. After being cooled, EB biochar was crushed and sieved to obtain a uniform size range of 2.0-3.0 mm and used as filter media (Figure 1a). To make the MEB (Figure 1b), the modification method was adapted from Taffarel and Rubio (2009) and Xuwen *et al*. (2010). EB (100 g) was placed in a 1000 ml beaker containing 500 ml of 5% (w/v) $K MnO_4$ solution prepared from $K MnO_4$ (AR grade, Qrec, New Zealand), then the mixture was heated at 90
80 and stimed for 4 hours. The mixture was then filened °C, and stirred for 1 hour. The mixture was then filtered to separate MEB, which was washed with tap water until the rinsed water was colorless. MEB was dried in an oven at 60 °C for 6 hours. Two commercial adsorbents, activated carbon (AC) (Figure 1c) and manganese green activated carbon (AO) (Figure 1d), and mangariese green
sand (Mn-G) (Figure 1d), were bought from a domestic supplier (J.L. Intertrade Co., Ltd.). The B was dreated at 90
C, and stirred for 1 hour. The mixture was then filtered
o separate MEB, which was washed with tap water until
the rinsed water was colorless. MEB was dried in an

Figure 1 Filter media: (a) eucalyptus biochar (EB), (b) modified eucalyptus biochar (MEB), (c) activated carbon (AC) and (d) manganese green sand. (b) modified eucalyptus biochar (MEB), (c) carbon (AC) and(d) manganese green sand. (b) modified eucalyptus biochar (MEB), (c) activated

Adsorbents were tested for adsorption capacity using the standard iodine adsorption method (ASTM D46070). Elemental analysis of adsorbent materials using a Rigaku ZSX Primus model, Wavelength Dispersive X-Ray Fluorescence Spectrometer (WDXRF), Model Rigaku ZSX Primus, Japan. Adsorbents were determined for the external surface structural morphology by scanning electron microscopy (SEM), JEOL Model JSM-7610F Plus.

2. The quality of groundwater

Groundwater was collected from a residential area in NonNhon subdistrict, Warinchamrap district, Ubon Ratchathani province. The pH of groundwater was in the range of 6.78 \pm 0.12, Iron and manganese concentrations of 0.354 \pm 0.022 mg/L and 0.723 \pm 0.002 mg/L, $\frac{1}{2}$ and $\frac{1}{2}$ a the maximum allowable concentration of 0.3 mg/L, groundwater quality for drinking purpose in Thailand. The total hardness was 420 \pm 0.5 mg/L as CaCO₃ which was classified as 'very hard' (Saha *et al.*, 2019). ectively. Mn concentrations were higher than
maximum allowable concentration of 0.3 mg/L,
ndwater quality for drinking purpose in Thailand. The
hardness was 420 ± 0.5 mg/L as CaCO₃ which was
ified as 'very hard' (Saha

3. Column adsorption set up

The filter column for manganese removal was set up using four types of filter media, consisting of EB, MEB , AC and MnG, which were run in duplicate. The $\frac{1}{2}$ size of glass column was 1 cm inner diameter and 76 cm bize of glass scremmed in the formal distribution and the only hard for 20 hardness was 420 \pm minutes to remove entrapped air in the pores (Ferrara, 1980). Then, 10 g of either EB, MEB, AC or 40 g of MnG were individually packed into a column to a height of 50 cm (Figure 2). The groundwater was continuously fed on (riguro L). The groundmater was committed, let samples were collected at delignated time (every hour for 24 hours) for Mn analysis. The breakthrough curve was plotted between the ratio of remaining manganese concentrations at various times and initial manganese $r = 1$ can be a size of the size mass. entration (Mn/Mn_0) and times.

cm inner diameter and 76 cm height. The filter

filter column system \mathbb{R}^n Figure 2 Schematic of filter column system **3. Mathematical models** Figure 2 Schematic of filter column system

4. Mathematical models ${\sf hematical\ models}$

4. mathematical models

The general mathematical equations for describing adsorption columns are Thomas and Yoon-Nelson models, which provide widely used data is theoretical methods to describe column performance (Chen *et al.*, 2012). The assumption of the Thomas **Result** model is based on the Langmuir kinetics of adsorptiondesorption with no axial dispersion. The rate driving force **1. Char** obeys second-order reversible reaction kinetics (Ayoob was 15 & Gupta, 2007). The model is described in Equation 1. Was 15 model is based on the Langmuir kinetics of adsorptionet al., 2012). The assumption of the Thomas model is based on the Langmuir model is based on the T The general mathematical equations maanomatical measus
The general mathematical equations for $k = 0$ of a direction-desorption-desorption-desorption-desorption-desorption-desorptionadition. The rate driving force observed the rate driving force observed and the rate driving force obeys seconda 2007). The model is described in Equation 1 theoretical methods to describe column performance
(Chen et al. 2012). The assumption of the Thomas desorption with no axial dispersion. The rate driving force performance (Chen et al., 2012). The model is described in Equation 1 of the Thomas model is based on the Langmuir model is based on the Langmuir model is based on the Langmuir model is $\mathcal{L}_\mathcal{D}$

$$
ln \frac{c_0}{c_t} - 1 = \frac{k_{Th}q_0 m}{Q} - k_{Th}C_0 t, \qquad (1)
$$

where C_o , C_t are initial Mn concentration and concentration at time t (mg/L), respectively. k_{Th} is a success Thomas constant (mL/min.mg), t is the total flow time (min), and Q is the volumetric flow rate (mL/min). images $\sum_{i=1}^{n}$ and $\sum_{i=1}^{n}$ is the voluments flow rate $\sum_{i=1}^{n}$, $\sum_{i=1}^{n}$, $\sum_{i=1}^{n}$ denoted as q_0 (mg/g) and m (g), respectively. Plot of where $C_{_{O}}$, $C_{_{t}}$ are initial Mn concentration and Adsorption capacity and mass of the adsorbent are images
denoted as $q \pmod{m}$ (n), respectively. Plot of adsorbe $\ln \frac{c_0}{c_t} - 1$ versus *t* gives the value of k_{Th} and q_0 . affect a η L), respectively. κ_{Th} is a α (a) respectively. Plet of adsorbe $\frac{1}{\sqrt{2}}$ ntration at time t (mg/L), respectively. k_{Th} is a as constant (mL/min.mg), i is the total flow time noted as q_0 (mg/g) and m (g), respectively. Plot of where σ_0 , σ_t are initial mate concentration and σ s constant (mL/min.mg), t is the total flow time concentration at time t (mg/L), respectively. $k_{\tau h}$ i

The Yoon-Nelson model is a simple model which does not require explicitly elaborated information. which does not require explicitly elaborated information.
50% of the breakthrough time can be predicted from the equation as expressed in Equation 2. (Yoon and Nelson, 1984). predicted from the expression as expressed in the expression of the expression \mathcal{L} the not require explicitly elaborated information.

$$
ln \frac{c_t}{c_{0-}c_t} = k_{YN}t - \tau k_{YN},
$$
\n(2)

 $\begin{bmatrix} 1 & 1 & 1 \\ 1 & 1 & 1 \\ 1 & 1 & 1 \end{bmatrix}$ adsorbate breakthrough (min) and *t* is time (min). The value of k_{yy} was calculated from the slope by plotting the graph between $ln \frac{C_t}{C_0 - C_t}$ $k_{_{\text{YN}}}$ is the rate constant (mn⁻¹), is time re and *t*. Where, k_{yy} is the rate constant (mn⁻¹), is time required for 50% potting the graph between $\ln \frac{C_t}{C_0 - C_t}$ and t. Where the rate constant (mn^{-1}) , is time required for 50% tting the graph between $ln \frac{c_t}{c_{0-}c_t}$ and t. Where,
the rate constant (mn⁻¹), is time required for 50% and t. Where, $\lim_{n \to \infty} f_n$ is the required for $\cos \theta$ $\frac{1}{\sqrt{2}}$, $\frac{1}{\sqrt{2}}$ and $\$ ing the graph between $ln \frac{C_t}{C_0-C_t}$ and t. Where, ie rate constant (mn `), is time required for 50%
ite breakthrough (min) and *t* is time (min).

5. Analysis and characterization

 $(PH < 2)$ after collection and then digested by nitric acid
filter column system water online

using microwave digestion. The digested samples were and the rate constant f_1 filtered through filter paper (Whatman no.42) and were $t_{\rm max}$ and $t_{\rm max}$ Water samples were acidified with nitric acid analyzed for manganese concentration using inductively coupled plasma-optical emission spectrometry (ICP-OES, model Optima 8000, Germany). The average of duplicate data is reported for each column. manganese concentration using inductively inductively inductively inductively inductively inductively inductive ed for manganese concentration using inductively
d plasma-optical emission spectrometry (ICP-OES, $\overline{\text{0}}$ on $\overline{\text{0}}$ on $\overline{\text{0}}$ (Germany) The average of duplicate purna 8000, Germany). The average of duplicate
conorted for each column

Results and discussion spectrometry plane digested samples were filtered through filtered through filtered through filters were paper paper.

1. Characterizations of the adsorbent

average of duplicate data is reported for each α was 152.42, 271.96, 174.67, 6.14 mg/g, respectively, indicating a low number of pores of MnG. Results from **coupled** plasma-optical emission spectrometry of the advancement of the WDXRF revealed that there were Mn in EB, AC, MEB and MDANT revealed that there were within ED, AO, MED and WDANT revealed that there were within ED, AO, MED and MEB had high Mn content after modification by $KMnO_4$ showing that insoluble manganese oxide (MnO_x(s)) was were many that models of many and or share successfully coated onto the EB surfaces. The iodine number of EB, AC, MEB and MnG acterizations of the adsorbent
The ieding number of EB AC MEB and MpC , and moor
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was successfully coated on the EB surfaces. The EB surfaces in the EB surfaces on the EB surfaces. The EB surfaces in the EB surfaces of the EB surfaces. The EB surfaces in the EB surface of the EB surfaces. The EB surface The external surface structure morphology images before adsorption are shown in Figure 3. The images show that there were pores on the surface of adsorbents, indicating their porosity. The main factors that affect adsorption capacity are particle size, pore diameter, and specific surface area (Wang *et al.*, 2010). detection capacity are perceity. The main receive that hecific surface area (Wang *et al.* 2010) before adsorption are shown in Fi
show that there were pores on the Sorption capacity are particle size, pore diameter,
sife surface area (Waren of al. 2040) $M_{\rm A}$ was 152.42, $(3,2,4)$, $(7,4)$

Figure 3 SEM images: (a) eucalyptus biochar (EB), (b) modified eucalyptus biochar (MEB), (c) activated carbon (AC) and (d) manganese green sand. Figure 3 SEM images: (a) eucalyptus biochar (ED),
(b) modified eucalyptus biochar (MFR) (c) activated

2. Manganese removal activated carbon (AC) and (d) manganese green

oxidation. $\text{MnO}_x(\text{s})$ on filter media surfaces of MEB and MnG cold oxidize $Mn(II)$ rapidly and $Mn(II)$ was also removed *via* adsorption until all available adsorption shes were occupied (Khocke et al., 1990). According to research on the removal of Mn using MnG, which has a MnO_x coating liked MEB on the filter surface. Manganese removal efficiency from each column ranged from 46.11-63.67%, 30.70-58.72%, 53.29-88.01% and $56.70-68.27%$, for EB, MEB, AC and MnG, and 56.70-68.27%, for EB, MEB, AC and MnG,
respectively at 1,440 min (Figure 4). 50% removal of manganese was achieved at for EB, MEB, AC, and MnG can be used to remove soluble Mn(II) in filters via column ranged from 46.11-63.67%, 30.70-58.72%, at 1,020, 240, 1,140 and 660 min, respectively. Mn(II) ard your, and state over many respectively. m_{A} , was removed by complexation or electrostatic attraction was removed by complexation or electrostatic attraction functional groups in EB (Wilamas *et al.*, 2022) and AC (Yin *et al.*, 2007, Omri & Benzina, 2012). MnG can be used to remove soluble Mn(II) in filters *via* sorption and sites were occupied (Knocke *et al.* 1990). According to sand.

 The breakthrough curve of each column was determined by plotting the ratio of Mn/Mn_{o} against time as shown in Figure 5.

Figure 5 Breakthrough curve

The Mn/Mn₀ ratios for all filter media except MEB did not achieve 0.95 until 5,000 min whereas the Mn/Mn $_{\tiny \odot}$ values of MEB were higher than 0.95 at 240 min and followed by MnG at 540 min. of EB was highest at 1,020 min. However, MEB and MnG filters gave high removal efficiencies during the initial period (0-240 min), due to the vacant surfaces of these adsorbents occurring in $M_1(0, 0, \ldots, M_n^{2+1})$ Mn(IV) oxide (MnO₂) form. Mn²⁺in groundwater is adsorbed $\overline{}$ $\lim_{z \to 0}$ on the surface of adsorbent, as shown in Equation 4. (Letterman, 1999). 1999). on the surface of adsorbent, as shown in Equation 4.
(Letterman, 1999)

$$
Mn^{2+} + MnO_2(s) \longrightarrow MnO_2(s) - Mn^{2+}
$$
 (4)

 The breakthrough curve enabled determination The breakthrough curve enabled The breakthrough curve enabled of the breakthrough time (t_b) . The amount adsorbed at breakthrough time is q_b . The length of the unused bed at breakthrough time is q_b . The length of the unused bed at breakthrough (L_m) is determined by equation 3 (Gabelman, 2017). σ 3 (Gabelman, 2017). 2017). The breakthrough curve enabled determinatior the breakthrough time (t_{b}) . The amount adsorbed a \sum_{m} is determined by equation of the mind.
17) efficiencies during the initial period (0 – 240 min),

$$
L_m = L \left(1 - \frac{t_b}{t_f} \right),\tag{3}
$$

where, L is the total bed length (cm), t_f is the midpoint of the real S-shaped breakthrough curve. midpoint of the real S-shaped breakthrough curve. midpoint of the real S-shaped breakthrough curve.

 However, the maximum allowable Mn However, the maximum allowable Mn However, the maximum allowable Mn concentration for drinking purpose is 0.3 mg/L, thus this concentration for drinking purpose is 0.3 mg/L, concentration for drinking purpose is 0.3 mg/L, present study used the 50% breakthrough time, as shown in Table 1. $\frac{1}{2}$

Filter media *t ^b t f* L_m q_b **(min) (min) (cm) (mg/g)** EB 1,020 1,938 23.68 1.278 MEB 240 300 10.00 0.342 AC 900 2,166 29.22 1.233 MnG 540 1,254 28.47 0.169

Table 1 The constant values from the breakthrough graph.

Table 2 shows the constant values of Yoon and Nelson model and Thomas model. The adsorption capabilities predicted by the Thomas model were in good agreement with the experimental results. The correlation coefficient (R^2) ranged from 0.8717 to 0.9709, indicating the best fit of the model with the experimental breakthrough curve. The Thomas model is suitable to describe the adsorption of manganese onto the filter media and aid in the design of columns with the best parameters. From this present study, the value of the Thomas constant (k_{TL}) of MEB was the highest, followed by MnG, which corresponds to the highest removal efficiencies of manganese during the initial period.

From the Yoon-Nelson model, (*τ*) the time of 50% adsorbed breakthroughs, was consistent with the time of the experiment (t_{exp}) . The R^2 values were relatively high (0.8197-0.9709), indicating that this model was effective at forecasting breakthrough time.

In this study, it was revealed that manganese had limited removal efficiency *via* its adsorption onto the adsorbent medium. The Mn removal was effective at alkaline pH values. According to Lefkowitz *et al*. (2013), dissolved Mn(II) is oxidized to insoluble forms of Mn(III) and Mn(IV) and then physically separated by filtration. Due to different removal mechanisms, EB and AC had a longer breakthrough time than MEB and MnG. The iodine number was high in EB and AC indicating adsorption into pores.

SEM pore size images of EB and AC confirmed pore size to be a factor in manganese adsorption. Furthermore, from the result of Fourier transform Infrared spectroscopy by Wilamas *et al*. (2022) reported the Mn adsorption by EB surfaces at the hydroxyl functional group.

It was found that the initial manganese removal efficiency of MEB and MnG was high, due to the oxidation and adsorption processes during first 120 min. MEB could not remove Mn after 250 min. This can be explained if the excess Mn on the MEB surfaces was leached out as the groundwater had a low Mn concentration of 0.723 mg/L. It can be seen from WDXRF that Mn content in MEB was 8 times that of MnG. In addition, the removal performance of adsorbents depends on adsorption conditions such as pH, Mn concentration and adsorbent dosage. It is recommended to use low amounts of MEB and MnG in the filter column as Mn may desorb in the case of the groundwater having a low Mn concentration. Biochar filters should be backwashed according to breakthrough time to remove the accumulated fine particles. However, spent biochar cannot be reused because its surface functional groups area was occupied *via* chemical adsorption (Wilamas *et al*., 2022). Thus, the combination with AC or EB filter media could enhance manganese removal efficiency.

The cost of the commercial grade of AC, MnG and KMnO₄ ranges from 95-120, 200-250 and 180 - 250 Baht /kg. The EB cost is 7.5 Baht/kg, while MEB cost is 8.13 Baht/kg. Thus, in comparison to MnG, EB should be developed further by using a smaller amount. In addition, use of these local materials can reduce the cost of water treatment for the community.

The literature-reported adsorption capacities (q) of Mn(II) onto EB and MEB were compared with those of other filter media, and the results are displayed in Table 3. According to the table, although EB and MEB could remove manganese, their efficiency was dependent on operating conditions.

Table 2 Parameters of Thomas and Yoon-Nelson models under column adsorption process.

Table 3 Comparison of Mn(II) adsorption capacity with other filter media.

Conclusions

This study evaluated the efficiency of fixed-bed adsorption columns using EB and MEB as filter media to remove manganese from actual groundwater. The results revealed that EB and MEB can be used as filter media. The manganese removal efficiency in EB and MEB were 63.67% and 58.72%, respectively, with the Mn concentration within the acceptable range at 0.3 mg/L. Both types of filters were equivalent to AC (88.01%) and MnG (68.27%). In addition, application with groundwater having different concentrations of manganese needs to be studied on a case-by-case basis.

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